1. Introduction

Zinc coated deep-drawing sheet is marketable in many industrial applications including first of all automotive industry. The barrier effect of zinc protects steel against corrosion in several environments [1, 2]. A light weight design, required mainly nowadays, is possible only with the application of higher strength steel, with maintained plastic properties, the latter essential for steel used in automotive industry. It can be obtained by the use of micro alloyed steel sheet, with micro alloying (under < 0.15%) applied together with controlled cooling rolling (thermo-mechanical treatment). For the increase of strength, grain refinement and precipitation strengthening is used. The grain refinement has a beneficial effect on plastic properties too, and it can offset the adverse effect of precipitation hardening [3, 4, 5]. Micro alloyed steel sheet has finer grain than usual steel sheet and that is why the criteria for plastic formability of the sheet are to be modified.

In this contribution the deep-drawing and fatigue properties of selected zinc coated steel sheet are analyzed. The increase of productivity in current press lines is sought in the increase of the pressing speed at first. It means the increase of the strain rate. Higher strain rate results higher resistance of the material to plastic deformation, and changes in the deformation process of the material [5, 6, 7]. As references show, up to a certain value of the strain rate the plastic deformation properties of the material do not change significantly, or the plasticity can even grow slightly [7, 8]. The intensity by which the strain rate can influence the plastic properties is strongly material dependent [4, 5].

The critical degradation mechanisms influencing the life of an automobile part are the fatigue and corrosion. Cyclic loading is frequently the main factor of surface damage and, on the other hand, surface damages can decrease fatigue properties significantly.

The aim of this contribution is the analysis of plasticity for selected deep drawing zinc coated micro alloyed steel sheet and the evaluation of the influence of strain rate on the analyzed properties, as well as to determine the fatigue properties and to monitor the behavior of the zinc layer during forming and fatigue life.

2. Experimental material and methods

Experimental test pieces were made from 2 mm thick stripes made of micro alloyed cold rolled steel which was hot zinc coated after rolling. The steel was grade H220YD (C < 0.01%, Al > 0.01%, Ti < 0.012%, Nb < 0.022%) and H380LAD (C < 0.15%, Al < 0.01%, Ti < 0.015%, Nb < 0.09%). The grade H220YD has actually a ferritic microstructure with the mean grain size of 0.016 mm (Fig. 1) and the grade H380LAD has ferrite with the mean grain size of 0.0056 mm with a small amount of pearlite (Fig. 2). Cut outs were made from the sheet and flat test pieces oriented in the direction of rolling were machined for tensile testing. The same was applied for the deep drawing Erichsen tests and fatigue tests in bending.

For static tensile tests a universal test machine INSTRON 1185 was used and this machine was used retooled with an Erichsen test fixture for the deep drawing tests in the press tool velocity interval from 3.3·10^{-3} m.s^{-1} to 1.0·10^{-3} m.s^{-1}. Deep drawing tests with ram speed of up to 2.5 m.s^{-1} were made in a drop weight tester. The fatigue properties of the steel sheet were tested in bending with symmetrical fatigue cycles at 35 Hz for the limit N_{f_c} = 10^7.
The behavior and integrity of the zinc coating layer was monitored in both macro and microscope.

3. Results and discussion

The tensile test results for the tested 2 mm thick sheet are in Tab. 1.

As shown in Tab. 1 the steel grade with higher strength (H380LAD) has the measured plasticity values lower ($A_{80}$, $n$) compared to the steel grade H220YD. The increased strength of steel grade H380LAD in comparison to grade H220YD is first achieved by the finer grain and precipitation strengthening due to the higher carbon content and micro alloying elements. According to the elongation values $A_{80}$, deformation strengthening exponent $n$, and the ratio $R_{p0.2}/R_m$ the steel grade H220YD sheet belongs into the group of deep drawing sheet, suitable for deep drawing. Steel grade H380LAD sheet cannot be put into this group for the obtained characteristic values. During plastic deformation for the steel grade H380LAD sheet a higher strengthening modulus $D$ was obtained, tested for the 10% part of the total deformation.

Basic information about the formability of the steel sheet can be obtained by tensile testing. However, the formability of the sheet is influenced by a number of factors arising from the production technology applied [7, 9, 10]. Important characteristics of formability can be obtained by technological tests. Tab. 2 presents the results of deep drawing Erichsen tests ($I_E$ – is the Erichsen number) at different press tool velocities.

Erichsen deep drawing test results for different press tool velocities $v$

<table>
<thead>
<tr>
<th>Steel Grade</th>
<th>$v$ [m.s$^{-1}$]</th>
<th>3.3. $10^{-3}$</th>
<th>8.3. $10^{-3}$</th>
<th>1.6. $10^{-2}$</th>
<th>2.10$^{-1}$</th>
<th>2.5</th>
</tr>
</thead>
<tbody>
<tr>
<td>H220YD</td>
<td>$I_E$ [mm]</td>
<td>12.5</td>
<td>12.6</td>
<td>13.0</td>
<td>12.7</td>
<td>11.2</td>
</tr>
<tr>
<td>H380LAD</td>
<td>12.4</td>
<td>12.5</td>
<td>12.6</td>
<td>12.5</td>
<td>11.5</td>
<td></td>
</tr>
</tbody>
</table>

Erichsen deep drawing test results showed that the indentation depth up to the fracture of the indented cup ($I_E$) is actually the same for both steel grades used, though they have large differences in elongation $A_{80}$. This can be caused due to difference in the stress distribution at the Erichsen deep drawing test and during tensile test.

The influence of the strain rate on the $I_E$ values is plotted in Fig. 3. As it can be seen, for the increase of the press tool velocity up to about $v = 0.2$ m.s$^{-1}$ there is a slight growth of the $I_E$, then there is a slight decrease of the $I_E$ value. For the highest velocity $2.5$ m.s$^{-1}$ the obtained value $I_E$ is the lowest. The turning point velocity $0.2$ m.s$^{-1}$ marking the start of the $I_E$ value decrease is roughly equivalent to the strain rate $1$ s$^{-1}$. The experiments are in good agreement with data reported in references [6, 7, 8], declaring that up to the strain rate of about $1$ s$^{-1}$ there is no significant decrease of steel sheet formability by the increase of the press tool velocity, and in this zone the traditional deep drawing criteria can be applied.

During testing and production by forming due to the heterogeneity of deformation the instant strain rate of a local spot is changing and can be different from the mean value calculated and can be significantly higher. The homogeneity of the plastic deformation is dependent on the microstructure of the steel sheet and
on the applied forming technology [4, 5]. The critical forming velocity depends on these factors, too.

The susceptibility of the material to influences caused by strain rate depends on the internal composition of the material. In generally, the higher homogeneity of the internal structure and the lower amount of barriers to the movement of dislocations causes that material is more sensitive to strain rate [4, 5]. Deep drawing test results show, too, as shown in Fig. 3 that the \( I_E \) value for steel grade H380LAD sheet (\( R_y = 382 \) MPa) is less susceptible to strain rate than steel grade H220YD sheet (\( R_y = 246 \) MPa).

The outstanding decrease of the \( I_E \) at impact forming (\( v = 2.5 \) m.s\(^{-1}\)) is due to different factors. We suppose that the decisive factor is heterogeneity of the plastic deformation distribution during the forming of the cup at very high strain rates and the deformation is localized in the critical parts of the cup. This can result in a decrease of the total value of plasticity. Changes of the friction between the tool and sheet can have influence, too.

For the service life in the car body the most important properties of pressed steel sheet parts are the resistance against fatigue and corrosion. They are stressed most frequently by alternating forces in bending. In Fig. 4 are plotted the dependences of the fatigue stress \( \sigma_h \) on the number of cycles to fracture \( N \), for symmetric cyclic bending of the tested steel sheet. The final fatigue limit and its rate to the UTS are the determined characteristics showing the quality of the resistance to fatigue. The fatigue limit of the steel grade H220YD in bending was \( \sigma_{C_0} = \pm 152 \) MPa and the rate to UTS was \( \sigma_{C_0}/R_m = 0.41 \). For the steel grade H380LAD it was \( \sigma_{C_0} = \pm 190 \) MPa and \( \sigma_{C_0}/R_m = 0.37 \), respectively. The tested characteristics and the slope of the decreasing Wöhler curve, (Fig. 4) assign both the tested steel grade sheets to ones with a good resistance to fatigue damage.

The increased corrosion resistance of the tested steel sheet is achieved by hot dip zinc coating. Damages of the integrity to the zinc coating layer during forming or service life decrease the corrosion resistance significantly, and can be an initiation spot of damage by fatigue [10, 11]. Macro and microscopic analyses of the tensile test pieces surface layer during tensile testing did neither reveal any damages of the coating nor any loss of cohesion to the steel base. Neither the other tests, the deep drawing Erichsen test and fatigue testing in bending showed damages to the coating. It is documented in Fig. 5 where the fracture surface of the sheet H220YD with the zinc surface layer is shown after cycling with stress equal to the fatigue limit \( \sigma_{C_0} \) and life to the limit of \( 10^7 \) cycles.

For the service life in the car body the most important properties of pressed steel sheet parts are the resistance against fatigue and corrosion. They are stressed most frequently by alternating forces in bending. In Fig. 4 are plotted the dependences of the fatigue stress \( \sigma_h \) on the number of cycles to fracture \( N \), for symmetric cyclic bending of the tested steel sheet. The final fatigue limit and its rate to the UTS are the determined characteristics showing the quality of the resistance to fatigue. The fatigue limit of the steel grade H220YD in bending was \( \sigma_{C_0} = \pm 152 \) MPa and the rate to UTS was \( \sigma_{C_0}/R_m = 0.41 \). For the steel grade H380LAD it was \( \sigma_{C_0} = \pm 190 \) MPa and \( \sigma_{C_0}/R_m = 0.37 \), respectively. The tested characteristics and the slope of the decreasing Wöhler curve, (Fig. 4) assign both the tested steel grade sheets to ones with a good resistance to fatigue damage.

Fig. 3 Influence of pressing tool velocity on Erichsen number \( I_E \) for investigated steel

The increased corrosion resistance of the tested steel sheet is achieved by hot dip zinc coating. Damages of the integrity to the zinc coating layer during forming or service life decrease the corrosion resistance significantly, and can be an initiation spot of damage by fatigue [10, 11]. Macro and microscopic analyses of the tensile test pieces surface layer during tensile testing did neither reveal any damages of the coating nor any loss of cohesion to the steel base. Neither the other tests, the deep drawing Erichsen test and fatigue testing in bending showed damages to the coating. It is documented in Fig. 5 where the fracture surface of the sheet H220YD with the zinc surface layer is shown after cycling with stress equal to the fatigue limit \( \sigma_{C_0} \) and life to the limit of \( 10^7 \) cycles.

4. Conclusion

Deep drawing and fatigue properties of two advanced deep drawing steel grades with yield points 246 and 382 MPa are analyzed in the contribution. The sheets were hot coated with zinc. The influence of the forming tool velocity on the deep drawing Erichsen test results are evaluated (the depth of the drawn cup at cracking).

The experimental results and discussion showed:

- The tested steel grades with increased strength and fatigue properties obtained by grain refinement and precipitation strengthening manifested very promising plasticity properties. The steel grade with high \( R_y = 382 \) MPa, though having a lower elongation at tensile testing \( A_{80} = 24\% \), had the Erichsen depth equal to the one for the steel grade with \( R_y = 246 \) MPa and \( A_{80} = 32\% \). A new approach is necessary to evaluate the deep drawing
properties of these steels if tensile test results are known only 
(A_{80}, n, R_y/R_m).
- The increase of the press tool velocity during forming (or at the 
  Erichsen test) up to about 0.2 m.s\(^{-1}\), which is equal to about 
  1 s\(^{-1}\) strain rate, results in a slight increase of the deep drawing 
  test result. Exceeding this velocity brings a decrease of deep 
  drawing properties; the decrease is more intense for the steel 
  with a lower yield point.

- The zinc surface layer retained integrity and cohesion to the 
  basic steel up to the final fracture of the tested piece by tensile 
  testing, Erichsen deep drawing tests, and fatigue tests.

Acknowledgement
This work has been supported by APVV Agency under No. 
APVV-0326-07

References