

Milan Stork *

SINUSOIDAL AND RELAXATION WIDE RANGE VOLTAGE CONTROLLED OSCILLATORS

This paper presents a sinusoidal Wien-bridge and square wave wide range voltage controlled oscillators. The square wave oscillator is based on relaxation (Schmitt trigger) topology. All described oscillators have potential use in different applications, e.g. phase locked loops, modulation and detection. The frequency changing is based on optically coupled resistor with 100 dB dynamic range. The oscillators were constructed and measured. The new method for amplitude control for quadrature oscillator is also described.

Keywords: Wien-bridge oscillator, relaxation oscillator, phase locked loop, voltage controlled oscillator, photoresistor, quadrature oscillator.

1. Introduction

A voltage controlled oscillator (VCO) is one of the important basic building blocks in analog and digital circuits. For example, a VCO is the main building block in phase locked loop (PLL) and clock generator circuits [1]. This paper presents the design of 2 types of oscillators that are continuously voltage tunable. The frequency changing for all oscillators is based on optically coupled photoresistor (Vactrol) with 100 dB dynamic range [2]. The first is Wien-bridge oscillator with frequency range from approx. 0.1 Hz to 250 kHz with sinusoidal output. The Vactrol

is used also for amplitude stabilization. The second oscillator is relaxation oscillator based on digital circuit with frequency range from 10 Hz to 9 MHz with square wave output. It is important to note that the control voltage and oscillator part are optically coupled.

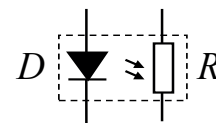


Fig. 1 The optically coupled photoresistor - Vactrol

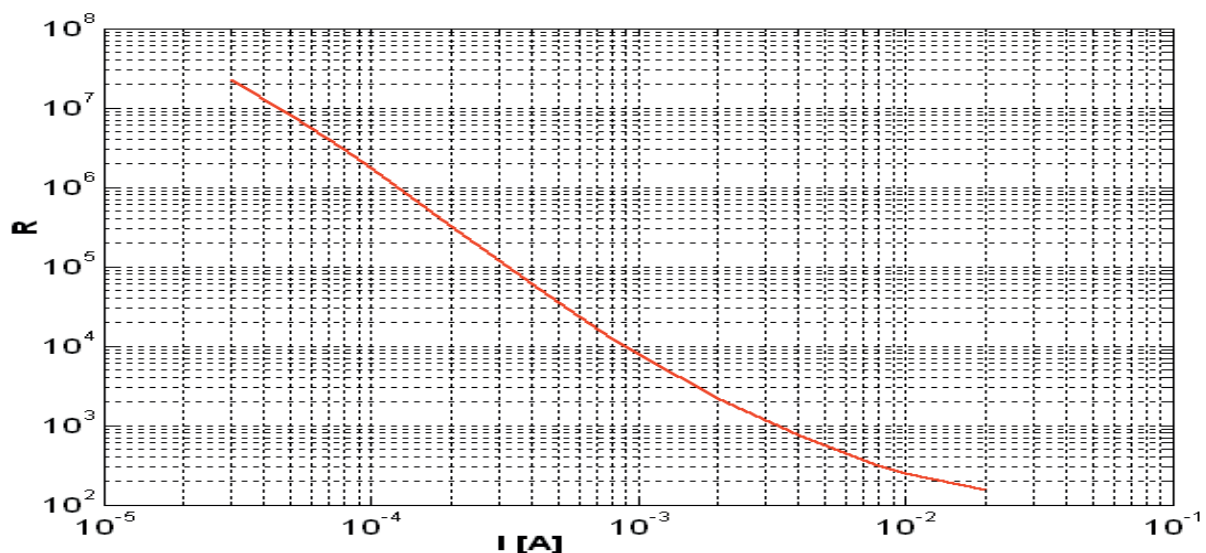


Fig. 2 Output resistance vs. input current for VTL5C1

* Milan Stork

Applied Electronics and Telecommunications/RICE, University of West Bohemia, Plzen, Czech Republic
E-mail: stork@kae.zcu.cz

2. Optically coupled photoresistor characteristic

Vactrol consists of a LED diode and photoresistor (Fig. 1). A photoresistor or light-dependent resistor (LDR) or photocell is a resistor whose resistance decreases with increasing light intensity. Optically coupled photoresistor (OR), also called photoresistive opto-isolator or Vactrol (after a trademark introduced by Vactec, Inc.) offers 100dB dynamic range, fast response time, and very high dark resistance. Some technical parameters for VTL5C1 [2] are: Min. isolation Voltage @ 70% Rel. humidity: 2500 VRMS; Max. resistor power: 175 mW; Max. resistor voltage: 100 V; Max LED current: 40 mA; Response time to 63% final R_{ON} 2.5 ms. The measured output resistance vs. input current is shown in Fig. 2 (logarithmic scales are used for both the X and Y axes).

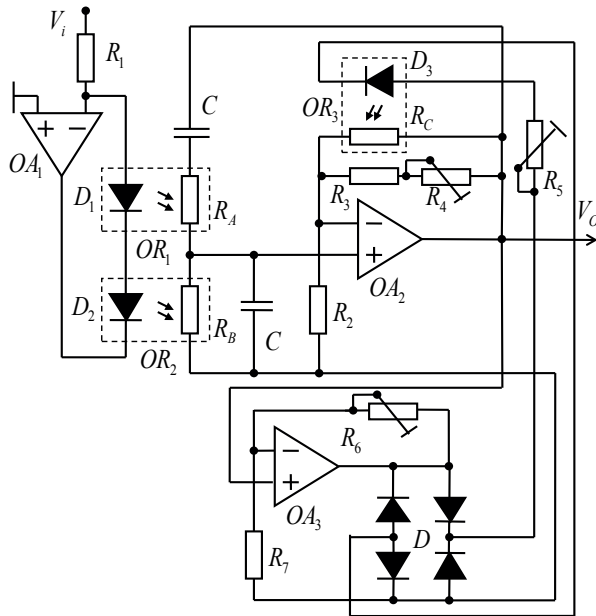


Fig. 3 The Voltage controlled Wien-bridge oscillator with buffer amplifier. $R_1=1k$; $C=1n$; $R_2=10k$; $R_3=15k$; $R_4=10k$; $R_5=1k$; $R_6=R_7=10k$; $OA=TL074$; D - 4x Schottky diodes, OR_1 - OR_3 optically coupled photoresistors VTL5C1.

3. Wide range voltage controlled Wien-Bridge oscillator

The voltage controlled Wien-bridge oscillator [3 - 5] is shown in Fig. 3. The operational amplifier OA_1 is used to form voltage controlled current source. The current i_D , flows through diodes D_1 and D_2 of the OR_1 and OR_2 . The output current is

$$i_D = \frac{V_i}{R_1} \quad [A, V, \Omega] \quad (1)$$

where V_i is input voltage and R_1 is resistor connected to inverting input.

The Wien-bridge oscillator consists of OA_2 where C ; R_A ; R_B are in positive feedback. The buffer OA_3 and diode bridge D , R_3 , R_4 , R_5 and OR_3 are used for automatic gain control. The output frequency is given as

$$f_o = \frac{1}{2\pi C \sqrt{R_A R_B}} \quad [Hz, F, \Omega] \quad (2)$$

Resistance of OR is approximately

$$R \approx \frac{k_{OR}}{i_D} = \frac{k_{OR}}{V_i/R_1} = \frac{k_{OR}}{V_i} \quad [A, V, \Omega] \quad (3)$$

where k_{OR} is OR constant and i_d is current through OR LED diode. Suppose that the $R_A=R_B=R$ in this case the output frequency is given by

$$f_o = \frac{1}{2\pi C \sqrt{R_A R_B}} = \frac{1}{2\pi C R} \approx \frac{V_i}{2\pi C R_1 k_{OR}} \quad [Hz, F, \Omega] \quad (4)$$

Measured output frequency vs. input voltage is shown in Fig. 4. The frequency spectrum is shown in Fig. 5 (spectral quality is better than 50 dB).

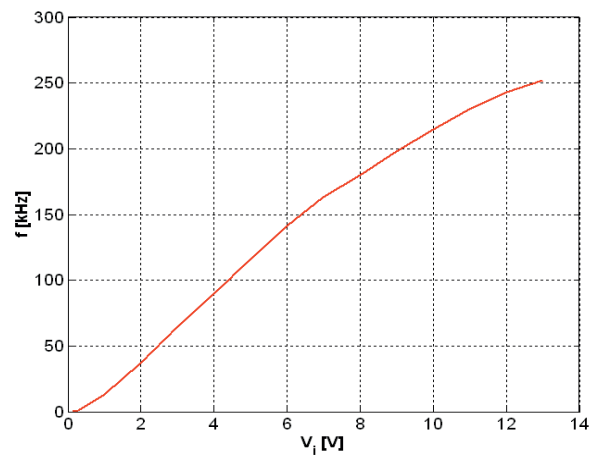


Fig. 4 Output frequency vs. input voltage for Wien-bridge oscillator

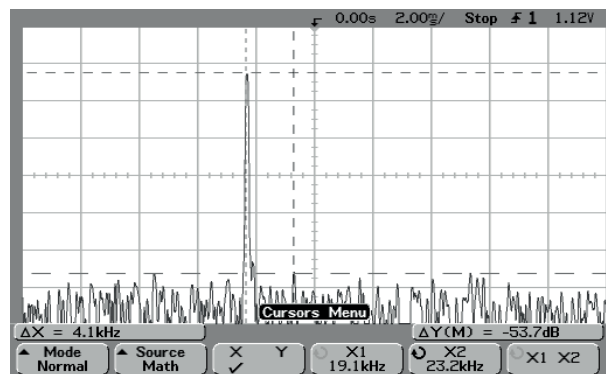


Fig. 5 The frequency spectrum of voltage controlled Wien-bridge oscillator

4. Amplitude control in quadrature sinusoidal oscillator

In this part another principle of the amplitude control of the quadrature sinusoidal oscillator is used. The block diagram of the quadrature oscillator with amplitude (energy) stabilization is presented in Fig. 6. The method is based on compensation of the parasitic dissipation parameters $-\alpha_1$ and $-\alpha_3$ by the multipliers connected in parallel along the dissipation blocks [6 and 7]. Desired value of the amplitude A of the oscillator signals is fed into the amplitude control block. The quadrature outputs of the oscillator (x_1 and x_2) are also connected to the amplitude control block. Amplitude control is based on eq. (5) where ideal steady state is

$$\begin{aligned} x_1^2 + x_2^2 &= (V_1 \sin(2\pi ft))^2 + (V_1 \cos(2\pi ft))^2 \\ &= V_1^2 (\underbrace{\sin^2(2\pi ft) + \cos^2(2\pi ft)}_1) = V_1^2 = A \end{aligned} \quad (5)$$

The amplitude is affected by means of PI (Proportional-Integrated) controller and multipliers controlled by x_3 .

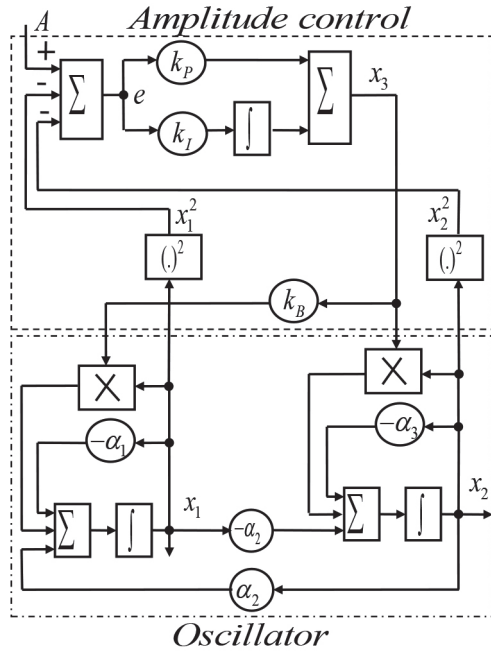


Fig. 6 Block diagram of the amplitude control for quadrature oscillator with compensation of dissipation α_1 and α_3 . Controller for amplitude control is based on PI controller

$$x_3 = k_p (A - x_1^2 - x_2^2) + k_i \int (A - x_1^2 - x_2^2) dt \quad (6)$$

and block k_b (in Fig. 6) is used for the balancing of different values of α_1 and α_3 . In Fig. 7 the block diagram of compensated integrator is shown (top) and compensated integrator with OA (bottom). The compensated integrator with OA can be described by eq. (7) where $R_f(i_d)$ is photoresistor controlled by current i_d .

$$\frac{V_i}{R_i} = -C \frac{dV_o}{dt} - \frac{V_o}{R_D} + \frac{R_3 R_4 (i_d) V_o}{R_2 (R_3 + R_4 (i_d)) R_5} \quad (7)$$

For ideal compensation of R_D

$$\frac{1}{R_D} = \frac{R_3 R_4 (i_d)}{R_2 R_5 (R_3 + R_4 (i_d))} \quad (8)$$

therefore,

$$R_4 (i_d) = \frac{R_2 R_3 R_5}{R_D R_3 - R_2 R_5} \quad (9)$$

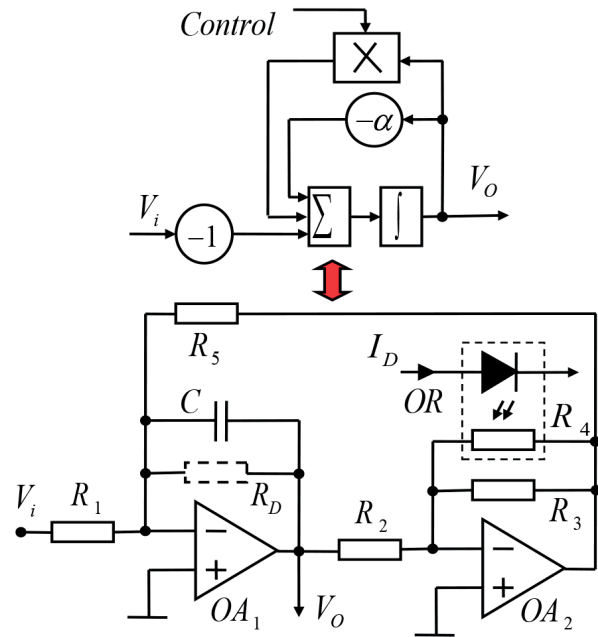


Fig. 7 The block diagram of amplitude control (top) and construction with optically coupled photoresistor (parasitic resistor R_D is compensated)

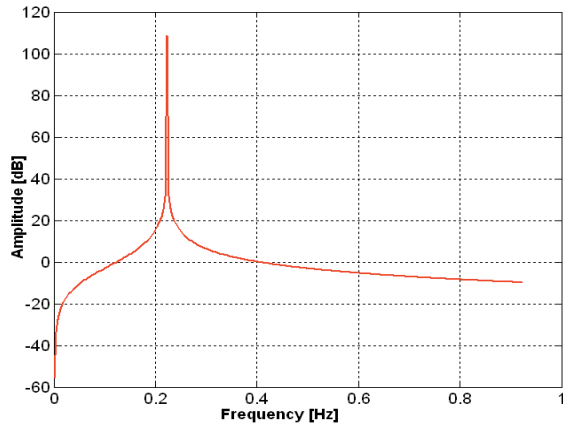


Fig. 8 Frequency spectrum of proposed oscillator (with compensation of the dissipation)

The frequency spectrum of quadrature oscillator with dissipative parameters compensation is shown in Fig. 8.

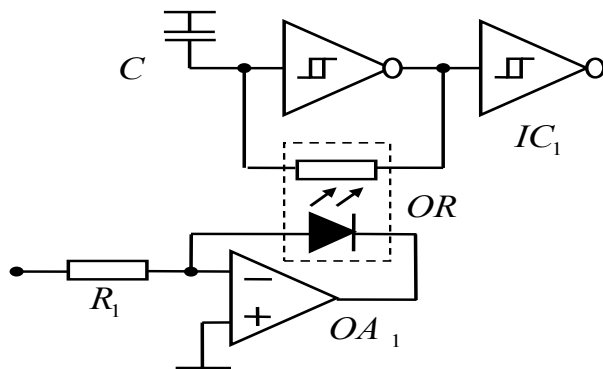


Fig. 9 The circuit diagram of relaxation oscillator with output buffer. $R_1=1k$; $C=56$ pF; OA -TL071; IC_1 -CD40109, OR - optically coupled photoresistors VTL5C1

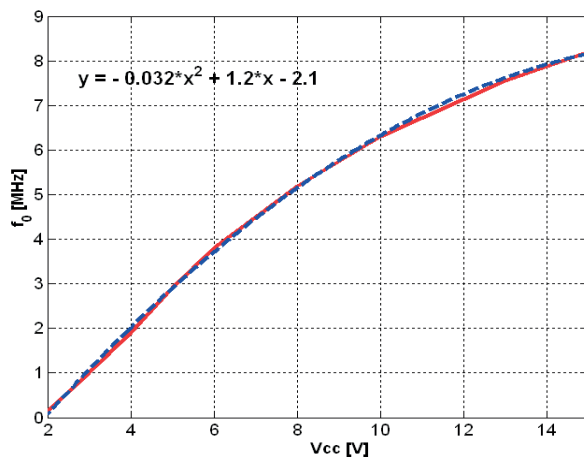


Fig. 10 Output frequency vs. supply voltage for relaxation oscillator with constant $V_i=13$ [V] (solid line), approximation - dash line

5. Wide range voltage controlled relaxation oscillator

The relaxation oscillator uses one Schmitt trigger capacitor and resistor [8 - 11]. The circuit diagram of voltage controlled relaxation oscillator with output buffer is shown in Fig. 9.

The output frequency vs. supply voltage (with fixed $V_i=13$ [V]) is shown in Fig. 10. The output frequency vs. input voltage (with fixed $V_{cc}=15$ [V]) is displayed in Fig. 11.

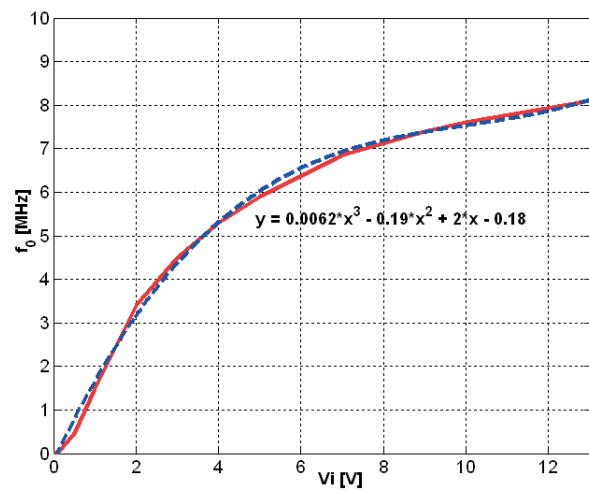


Fig. 11 Output frequency vs. input voltage for relaxation oscillator with $V_{cc}=15$ [V] (solid line), approximation - dash line

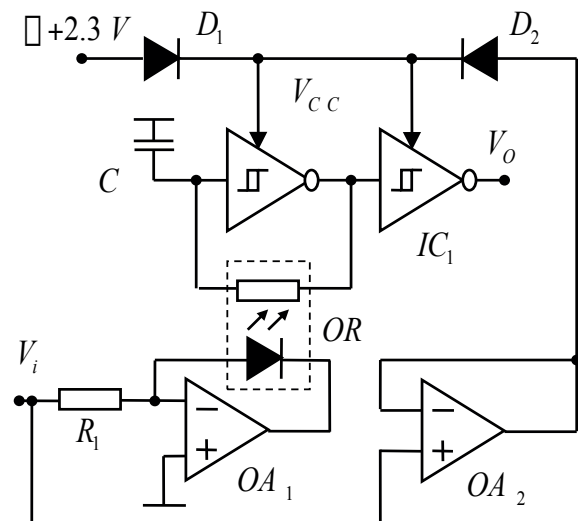


Fig. 12 The circuit diagram of linearized, relaxation oscillator with output buffer. $R_1=1k$; $C=56$ pF; OA_1, OA_2 -TL072; IC_1 -CD40109, D_1, D_2 - Schottky diodes, OR - optically coupled photoresistors VTL5C1

Measured values of output frequency versus input voltage for linearized relaxation oscillator

Table 1

V_i [V]	2	3	4	5	6	7	8	9	10
f_o [MHz]	0.12	0.9	1.7	2.6	3.5	4.3	5	5.8	6.4

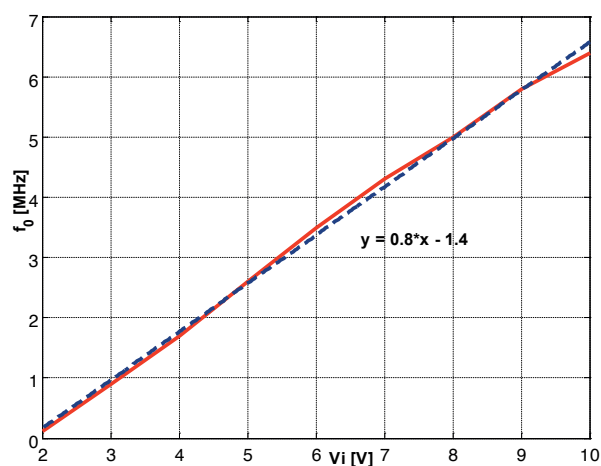


Fig. 13 Output frequency vs. input voltage for linearized relaxation oscillator (see Fig. 12). Measured values – solid line, approximation – dash line

The circuit diagram of linearized relaxation oscillator with output buffer is shown in Fig. 13. Linearization is based on supply voltage increasing together with input voltage. The OA_2 is used as power source for $V_i \geq 2.3$ V. The supply voltage is given by eq. (10):

$$V_{ss} = \begin{cases} \approx 2.3 & \text{if } V_i < 2.3 \\ V_i & \text{if } V_i \geq 2.3 \end{cases} \quad [\text{V}] \quad (10)$$

Output frequency vs. input voltage of the linearized oscillator is displayed in Fig. 13. Measured values are in Table 1.

6. Conclusion

In this paper the 2 wide range simple V-f oscillators were described. For frequency control, the optically coupled photoresistor was used. The first is Wien-bridge oscillator with sinusoidal output with spectral quality greater than 50 dB. The second is linearized relaxation oscillator. All oscillators were constructed and measured. It is important to note that these oscillators can be used in different applications including PLL, frequency locked loop and low cost frequency synthesizers. The new method for amplitude control of sinusoidal quadrature oscillators with high spectral quality based also on optically coupled photoresistors and PI controller was also described.

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